

ACADEMICIA A n I n t e r n a t i o n a l M u l t i d i s c i p l i n a r y R e s e a r c h J o u r n a l

(Double Blind Refereed & Peer Reviewed Journal)

DOI: 10.5958/2249-7137.2021.02250.3

AN EVALUATION OF BIOMASS GASIFICATION MODELLING

Dr Durgesh Wadhwa*

*SBAS, Sanskriti University, Mathura, Uttar Pradesh, INDIA Email id: hodchem@sanskriti.edu.in

ABSTRACT

Corn fermentation competes with the world food supply, while sugarcane fermentation contributes to deforestation. As a result, even if it is economically possible, the renewable and sustainable development of these two bio-based energy sources may not be desired. Biomass gasification, on the other hand, is far more versatile in terms of the bio-feedstock or waste that may be used to create biofuels or co-generate power and heat on demand. Downdraft gasifiers are well-suited for small-scale heat and power co-generation, whereas fluidized bed and entrained flow gasifiers currently reach promising economies of scale for fuel production. The frequency of different modeling options used, as well as the patterns shown by this data, are presented. This article offers a concise guide to the modeling decisions that must be made early in a modeling study or project for novice researchers. A comprehensive technique characterization is presented, which includes important modeling decisions that have not been clearly addressed in previous assessments. This survey gives seasoned researchers their first statistical snapshot of what their peers are working on.

KEYWORDS: *Biomass Gasification Equilibrium model Stoichiometric model Kinetic model Tar.*

INTRODUCTION

The main three fossil fuels now provide approximately 80 percent of the world's primary energy needs. Biomass and trash make up the second largest contribution, accounting for around 9%. Nuclear, hydropower, and the trio of fast increasing renewables geothermal, solar, and wind provide the rest of the world's energy requirements. The use of fossil fuels to generate energy has severe social, political, and environmental consequences, as fossil fuel combustion has raised

global concentrations and accelerated climate change. These ramifications are powerful motivators for the development of renewable and locally accessible energy sources. Biochemical and/or thermo chemical procedures are required to recover energy from biomass or organic solid waste. Biomass is transformed to biofuels via the digestive activity of living organisms during biochemical processes like fermentation[1]. Thermo chemical processes, on the other hand, use heat and/or pressure to transform biomass into biofuels, gases, and chemicals. Gasification, which is also often used to gasify coal and natural gas, is the most well-known thermochemical biomass-to-energy and waste-to-energy conversion process, and it is attracting increasing scientific and commercial attention. Gasification, in comparison to more traditional methods such as incineration, produces syngas from biomass for future biofuel synthesis and generally achieves higher power generation efficiency $[2]$. When compared to alternatives such as incineration or biogas from digesters, gasification recovers more power per kilogram of biomass or per kilogram of municipal garbage. With current or little changed infrastructure, energy may be produced from syngas using gas engines, gas turbines, or fuel cells.

There is currently a large body of work that uses models of several kinds of gasifiers with varying degrees of sophistication. However, there are few reviews of these modeling and simulation research. Our search yielded seven more evaluations, which would seem to be adequate if not for the fact that many of them are very similar[3]. There is a specific need for reviews that evaluate modeling methods and address key questions about what is known about the relative advantages of various modeling approaches, rather than just listing kinds of models and previous research. For example, the present study is the first to look at whether stoichiometric and nonstoichiometric models provide the same results. The current study is also the first to address one of the most important decisions a modeler must make: whether to adopt a complete equilibrium or semi-equilibrium method[4]. The inclusion of sample data showing the frequency of usage of the different competing modeling options in the literature to date is another aspect of the current research that sets it apart from previous studies.

Figure 1:Flow diagram depicting the details of the literature search.

This section explains how the systematic search approach (shown in Fig. 1) was used to select articles for inclusion in the review's statistics and comments. To begin, keywords gasification and modeling or modeling were searched in three databases: Google Scholar, Ardabil Science, and Science Direct. Further evaluation of eligibility based on full-text publications resulted in the selection of 54 research, including 33 thermodynamic equilibrium models, 15 kinetic models, and 6 kinetic/equilibrium (CRF) models. One goal of the present study was to get a better grasp of how common these methods are.

Figure 2:Overview of gasification models since 2000, (a) as percent, (b) absolute number of studies

> ACADEMICIA: An International Multidisciplinary Research Journal https://saarj.com

Gasification process and technologies

Gasification process overview

The combustion of solid or liquid fuel into syngas is known as gasification. Syngas may be used as a chemical feedstock or directly as a fuel to produce heat, power, or both. The phases of the gasification process are: drying, pyrolysis, oxidation, reduction, and cracking (Fig. 3). The moisture content of biomass feed typically varies from 5 to 35 percent, but it is decreased to less than 5 percent throughout the drying process. The biomass is heated from 200 to 700 °C in the pyrolysis phase with little oxygen or air. The volatile components of the biomass are evaporated under these circumstances. Furthermore, the hydrogen in the biomass may be oxidized, resulting in the production of water[5]. The reduction processes that take place within the gasifier are endothermic, and the energy needed for them comes from the burning of char and volatiles. Through a series of processes, biomass reduction produces combustible gases such as hydrogen, carbon monoxide, and methane; the major reactions in this subcategory are as chooses to follow:

Figure 3: Gasification process steps

Biomass gasification technologies Fixed beds and fluidized beds are the two most common kinds of gasifiers.

- Fixed-bed: Gasifiers having a bed filled containing solid fuel particles and the gasifying medium and gas ascending, descending, or migrating horizontally through the reactor are classified as fixed-bed gasifiers. Air, steam, oxygen, or a combination of these may be used as the gasifying medium. When compared to fluidized bed alternatives, fixed-bed gasifiers have two major practical advantages: they are substantially more cost-effective for smallscale applications and they generate a clean product gas with minimal dust and tar content.
- The fluidized bed: A fluidized bed is a cylindrical column that holds particles and flows fluid across it. The fluid's velocity is high enough to suspend the particles inside the column, resulting in a wide surface area for the fluid to touch, which is the main benefit of fluidized

beds. Fluidized beds' primary potential benefits are better heat and material transmission between the gas and solid phases.

Fluidized bed generators and entrained flow digester seem to be the most viable options for biofuel production facilities among these gasifier types[6]. Downdraft gasifiers have emerged as the most appropriate choice among gasifier types for small-scale distributed power generation.

Models for biomass gasification

Equilibrium and kinetic models are the two major types of gasification models. According to this study of gasification modeling options, about 60% of biomass gasification simulations use an equilibrium model, while the remaining 30% use a kinetic model. The major variants of both of these methods will be discussed in this part, but first a short overview of the reasons for modeling and simulating biomass gasification will be discussed. Furthermore, the advantages and disadvantages of various techniques are collected[7]. To obtain a desired syngas composition and production, a gasification plant operator must optimize the feedstock flow rate, agent flow rate, equivalence ratio, reactor pressure, and temperature. Any of these variables may have a significant effect on the product compositions and gasifier performance.

Furthermore, since the chemistry and fluid dynamics of gasification are very sensitive to changes in feedstock composition, moisture, ash content, particle size, and density, the permissible range for feedstock characteristics is relatively limited. In reality, laboratory experiments, pilot facilities, and field experience may and do give knowledge on the best conditions and feedstock for a reactor, but these lessons are often more time-consuming and costly than modeling.

Models of thermodynamic equilibrium

Based on the premise that the components react in a completely mixed state over an indefinite length of time, the thermodynamic equilibrium method predicts the composition of the output gases.

When compared to kinetic models, thermodynamic equilibrium calculations are simple and independent of gasifier design. In the simplest, most ideal case, general thermodynamic properties can be used for equilibrium modeling, whereas kinetic modeling requires a larger set of difficult-to-find and accurate kinetic parameters.

Figure 4:A categorization of gasification model types.

ACADEMICIA: An International Multidisciplinary Research Journal https://saarj.com

Stoichiometric vs non-stoichiometric models

Stoichiometric and nonstoichiometric models are the most often mentioned subcategories of equilibrium models. According to this study and a complementary more thorough theoretical examination of the S versus NS technique elsewhere, the NS method is used in about 70% of equilibrium simulations in the literature, while the S method is used in the remaining 20%. S and NS models, on the other hand, provide almost similar predictions in practically all actual biomass gasification situations, as has been thoroughly shown elsewhere. As a result, the second classification proposed in this paper, namely Eq-single and Eq-separate models, is more important. The yield and product composition anticipated by the model are usually affected by the model option between an Eq-sing and an Eq-sep. Given these facts, it's possible that past evaluations and research have paid too much attention to a model choice that has little impact on model prediction. The equilibrium of a preselected set of reactions is computed in the stoichiometric case, while the equilibrium of a preselected set of chemical species is computed in the nonstoichiometric case[8].

The nonstoichiometric technique has the following specific steps:

1. Make a list of all of the species that will be included in the simulation (in principle, all the chemical species that the modeler deems might be in the gasifier effluent in non-negligible amounts)

2. Then, for a particular feed composition (which may be described simply as the elemental composition of the feed at the reaction temperature and pressure), calculate the resultant minimal Gibbs energy distribution among all these chemical species.

Models that are eq-single vs. models that are eq-separate Consistent framework may be categorized as Eq-sep or Eq-sing methods, in conjunction to stoichiometric or nonstoichiometric. This classified based about whether the char detonation is modeled as achieving a distinguishable balance point independent of the reduction of the VM and un-combusted char, as in the Eq-sep situation, or whether the combustion and reduction reactions achieve a single global equilibrium as one reactive chemical system, as in the case of the Eq-sep scenario.

LITERATURE REVIEW

Massimiliano Materazzi studied the most significant barrier to using fluid bed gasification for waste treatment is tar generation and ash disposal, which can only be met with expensive cleaning systems and additional processing. Any use of plasma in a different heat process allows for efficient crack propagation of complex organic life to primary synthesis gas constituents while lowering electric power consumption. This research looked at the advantages of a twostage thermal methodology over a single-stage approach in terms of thermodynamics. The simple truth that the foremost thermal waste decomposition is carried out in conditions of optimized stoichiometric ratio for the gasification reactants is one of them. Besides which, staggering the oxidant injection into two separate intake levels improves the system's efficiency and lowers plasma power consumption. After the two-stage process, a flexible model capable of providing reliable quantitative predictions of product yield and composition has been developed. This same method follows a systematic structure that incorporates atom conservation principles and equilibrium calculation routines, taking into account all conversion stages from waste feed to final products. Experimental data from a demonstrator plant was also used to verify the model.

The study successfully demonstrated that a multiple gasification system improves the system's gas yield and carbon conversion efficiency, both of which are critical in single-stage systems, while simultaneously increasing performance parameters[9].

Marco Formica studied the Aspen plus was used to create a novel steady-state zero-dimensional simulation model for a full-scale woody biomass gasification facility with fixed-bed downdraft gasifier. The model takes into account the technical features of all of the plant's components and operates in line with the plant's current primary control logics. The simulation findings are consistent with those found during a large-scale experiment. Following model validation, the effect of operational factors such as the equivalent ratio, biomass moisture content, and producer gas air temperature on syngas composition was investigated in order to evaluate the experimental plant's operative behavior and energy performance. It is feasible to achieve greater values of the gasifying air temperature and an increase in overall gasification performance by recovering the sensible heat of the syngas at the gasifier's output[10].

DISCUSSION

Even if the study is attempting the more difficult job of developing a kinetic model, it may be prudent to additionally run an equilibrium model for the same application. Equilibrium may play the same function in gasification as it does in any other chemical system, showing the thermodynamic limitations of operation and how they are affected by operating parameters and inputs. The inability to assess the effect of hydrodynamic factors on gasification when simply utilizing equilibrium modeling is a disadvantage. A kinetic model is needed if the aim is to optimize or understand the impact of factors such particle size distributions, feed density, and reactivity on the output gas composition, carbon conversion, and system performance. However, kinetic models often include difficult-to-find kinetic and transport parameters. Even if these parameters are measured, the resultant model will be constrained to the particular gasifier sort and design, feedstock, agent, and operating range combination wherein the rate expression form associated parameter values are valid to some extent.

CONCLUSION

A new categorization of the most significant gasification modeling methods was provided, as well as representative data on their usage frequency. But even though the best model to use relies on a variety of variables like the simulation's objectives, the kind of gasifier, feedstock, and operating parameters, a few basic conclusions may be made. Equilibrium models, in particularly, are an excellent place to start when modeling downdraft gasification. Along with its relatively simple shape and the relatively high operating temperature they usually utilize, downdraft gasifiers often function close to equilibrium. Additionally, both pyrolysis and gasification products are pushed through the oxidation zone with downdraft gasifiers, resulting in equilibrium after a short time. Due to the obvious critical significance of tar avoidance in creating viable and ecologically acceptable biomass and waste gasification technologies, tar modeling is expected and become one of the greatest active areas of study. The most pressing issue facing the biomass gasification modeling community is developing modeling methods that can sufficiently offer scientific understanding and/or practical operator advice here about how to control tar formation.

ACADEMICIA

REFERENCES

- **1.** D. Baruah and D. C. Baruah, "Modeling of biomass gasification: A review," *Renewable and Sustainable Energy Reviews*. 2014, doi: 10.1016/j.rser.2014.07.129.
- **2.** M. Hawrot-Paw, A. Koniuszy, M. Mikiciuk, M. Izwikow, T. Stawicki, and P. Sędłak, "Analysis of ecotoxic influence of waste from the biomass gasification process," *Environ. Sci. Pollut. Res.*, vol. 24, no. 17, pp. 15022–15030, 2017, doi: 10.1007/s11356-017-9011-8.
- **3.** A. Gómez-Barea and B. Leckner, "Modeling of biomass gasification in fluidized bed," *Progress in Energy and Combustion Science*. 2010, doi: 10.1016/j.pecs.2009.12.002.
- **4.** G. Mirmoshtaghi, H. Li, E. Thorin, and E. Dahlquist, "Evaluation of different biomass gasification modeling approaches for fluidized bed gasifiers," *Biomass and Bioenergy*, 2016, doi: 10.1016/j.biombioe.2016.05.002.
- **5.** S. Sharma and P. N. Sheth, "Air-steam biomass gasification: Experiments, modeling and simulation," *Energy Convers. Manag.*, 2016, doi: 10.1016/j.enconman.2015.12.030.
- **6.** R. Mikulandrić, D. Böhning, R. Böhme, L. Helsen, M. Beckmann, and D. Lončar, "Dynamic modelling of biomass gasification in a co-current fixed bed gasifier," *Energy Convers. Manag.*, 2016, doi: 10.1016/j.enconman.2016.04.067.
- **7.** K. Weber, T. Li, T. Løvås, C. Perlman, L. Seidel, and F. Mauss, "Stochastic reactor modeling of biomass pyrolysis and gasification," *J. Anal. Appl. Pyrolysis*, 2017, doi: 10.1016/j.jaap.2017.01.003.
- **8.** Q. Miao, J. Zhu, S. Barghi, C. Wu, X. Yin, and Z. Zhou, "Modeling biomass gasification in circulating fluidized beds," *Renew. Energy*, 2013, doi: 10.1016/j.renene.2012.08.020.
- **9.** M. Materazzi, P. Lettieri, L. Mazzei, R. Taylor, and C. Chapman, "Thermodynamic modelling and evaluation of a two-stage thermal process for waste gasification," *Fuel*, vol. 108, pp. 356–369, 2013, doi: 10.1016/j.fuel.2013.02.037.
- **10.** M. Formica, S. Frigo, and R. Gabbrielli, "Development of a new steady state zerodimensional simulation model for woody biomass gasification in a full scale plant," *Energy Convers. Manag.*, vol. 120, pp. 358–369, 2016, doi: 10.1016/j.enconman.2016.05.009.