DEVELOPMENT OF ALGORITHM AND PROGRAMS FOR TWO-DIMENSIONAL FILTERING PROBLEMS OF INCOMPRESSIBLE LIQUIDS

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ABSTRACT

The paper presents the task of controlling the filtration process of oil and gas fields. A computer model has been created for controlling filtration processes using mathematical models of the oil and gas field development process. With the help of the created model, the permeability, viscosity, porosity and production were selected to a minimum of the differences between the computational and actual pressures. Certain optimal parameters are used for control and forecasting in the development of oil and gas fields.

KEYWORDS: Field, Control, Control Task, Oil, Gas, Model, Mathematical Model, Wells, Permeability, Filtration, Equations, Viscosity, Porosity, Reservoir.

1. INTRODUCTION

Trends in the development of the oil and gas industry imply the introduction of modern innovative ways of development that ensure economic efficiency at every stage from hydrocarbon exploration to their final implementation. The transition to an innovative way of development in the geological and oil and gas industries involves the technical re-equipment of the means of obtaining geological information, its processing, interpretation and provision for use at all stages from prospecting to the final development of deposits. One of the main stages of increasing innovative ways of developing geological exploration and development of oil and gas condensate fields is the introduction of full-scale innovative technologies for the study of the subsoil of oil and gas fields and their development. One of the main elements of this is threedimensional geological and geophysical modeling at all stages from prospecting to field development and complex processing of GIS materials based on the latest programs. A threedimensional geological and geophysical model allows a more reliable representation of the geological structure of the field, the production and refinement of hydrocarbon reserves and the preparation of the basis for hydrodynamic modeling of the field. In hydrodynamic calculations associated with the development of oil and gas fields, which are arbitrarily located in the earth's crust, one-dimensional approximations are insufficient. This largely depends on taking into account the non-uniform nature of the flow in the system of many wells. [1-10]

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2. STATEMENT OF THE PROBLEM.

The mathematical formulation of a two-dimensional problem is reduced to the following. Let there be a reservoir with an area D. It is used to improve the dynamic viscosity μ . It is sealed using randomly applied wells with coordinates x and y in the mode of specified volumetric flow

rates $Q_i(t)$.

Using Darcy's law, the equation of continuity and state, we obtain the power-averaged twodimensional equation of fluid filtration, taking into account internal effluents:

$$\begin{cases} \frac{\partial}{\partial x} \left(K(x, y) \frac{\partial P(x, y, t)}{\partial x} \right) + \frac{\partial}{\partial y} \left(K(x, y) \frac{\partial P(x, y, t)}{\partial y} \right) = M(x, y) \frac{\partial P}{\partial t} + F(x, y, t) \\ \{(x, y) \in D, t > 0\} \end{cases}$$
(1)

at the initial

$$P(x, y, t)\Big|_{t=0} = P^{0}(x, y)$$
(2)

and the boundary condition along the contour:

$$\frac{\partial P(x, y, t)}{\partial n}\Big|_{(x, y)\in\Gamma} = 0$$

$$P(x, y, t)\Big|_{(x, y)\in\Gamma} = P_R(t)$$
,
(3)

where, *P* - is the pressure, $K = h \frac{k}{\mu}$, *k* - is the permeability of the formation, μ - is the viscosity of the fluid, $M = mh\beta_{\mu}^{*}$, *h* - reservoir thickness, *M* - porosity, β_{μ}^{*} - reservoir fluid elasticity, $F = Q_{i}(t) \cdot \delta(x - x_{i})(y - y_{i})$, δ - is the Dirac delta function.

To calculate problem (1) - (3), we pass to the dimensionless variables:

$$\overline{K} = \frac{K}{K_x}, \quad \overline{x} = \frac{x}{L_x}, \quad \overline{y} = \frac{y}{L_y}, \quad \overline{H} = \frac{H}{H_x}, \quad Q = A \sum_{i=1}^N \delta(x - x_i, y - y_i) q_i, \quad t = \tau \frac{K_x}{\beta^* \cdot L_x^2}.$$
(4)

3. SOLUTION METHOD.

To solve the dimensionless problem, we use one of the following schemes of the finitedifference method:

- 1. Longitudinal-transverse scheme [1].
- 2. Locally one-dimensional scheme [2].
- 3. Splitting [3].

To do this, cover the given area with a uniform mesh:

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$$\omega_{x,y} = \{ (x_i = i \cdot h_x, h_x = \frac{1}{N_x} | y_j = j \cdot h_y, h_y = \frac{1}{N_y}), i = \overline{1, N_x}, j = \overline{1, N_y}, \}.$$

Then the finite-difference form of the given problem will take the form

$$m_{i,j} \frac{H_{i,j}^{k+1} - H_{i,j}^{k}}{\tau} = \left(K_{i+1/2,j} \frac{H_{i+1,j}^{k} - 2H_{i,j}^{k} + H_{i-1,j}^{k}}{h_{x}^{2}}\right) + \left(K_{i,j+1/2} \frac{H_{i,j+1}^{k} - 2H_{i,j}^{k} + H_{i,j-1}^{k}}{h_{y}^{2}}\right) - Q_{i,j} \cdot$$
(5)

For convenience, we will write it like this:

$$A_i H_{i-1} - C_i H_i + B_i H_{i+1} = -F_i . (6)$$

To solve equation (5), we use a longitudinal-transverse scheme using the method in the version of a conventional sweep in a chain of one-dimensional equations. A_i , B_i , C_i , F_i take the following form:

$$A_{i} = B_{i} = \frac{K_{i+1/2,j}}{h_{x}^{2}}; \quad C_{i} = A_{i} + B_{i} + m_{i,j}\frac{2}{\tau}; \quad F_{i} = m_{i,j}\frac{2}{\tau}H_{i,j}^{k} + \left(K_{i+1/2,j}\frac{H_{i,j+1}^{k} - 2H_{i,j}^{k} + H_{i,j-1}^{k}}{h_{y}^{2}}\right) - Q_{i,j},$$

$$A_{j} = B_{j} = \frac{K_{i,j+1/2}}{h_{y}^{2}}; \quad C_{j} = A_{j} + B_{j} + m_{i,j}\frac{2}{\tau}; \quad F_{j} = m_{i,j}\frac{2}{\tau}H_{i,j}^{k+\frac{1}{2}} + \left(K_{i,j+1/2}\frac{H_{i+1,j}^{k+\frac{1}{2}} - 2H_{i,j}^{k+\frac{1}{2}} + H_{i-1,j}^{k+\frac{1}{2}}}{h_{x}^{2}}\right) - Q_{i,j}.$$
(7)

When applying the locally one-dimensional scheme, Ai, Bi, Ci, Fi take the form:

$$A_{i} = B_{i} = \frac{K_{i+1/2,j}}{h_{x}^{2}}; \quad C_{i} = A_{i} + B_{i} + m_{i,j}\frac{2}{\tau}; \quad F_{i} = m_{i,j}\frac{2}{\tau}H_{i,j}^{k} - Q_{i,j},$$

$$A_{j} = B_{j} = \frac{K_{i,j+1/2}}{h_{y}^{2}}; \quad C_{j} = A_{j} + B_{j} + m_{i,j}\frac{2}{\tau}; \quad F_{j} = m_{i,j}\frac{2}{\tau}H_{i,j}^{k+\frac{1}{2}} - Q_{i,j}.$$
(8)

Calculating the equations using the splitting method, we get the following sequences:

$$K_{i+1/2,j} \frac{H_{i+1,j}^{k-\frac{2}{3}} - 2H_{i,j}^{k-\frac{2}{3}} + H_{i-1,j}^{k-\frac{2}{3}}}{h_{x}^{2}} = m_{i,j} \left(\frac{H_{i,j}^{k-\frac{2}{3}} - H_{i,j}^{k-1}}{0.5\tau} \right), \quad 1) A_{i} = B_{i} = \frac{K_{i+1/2,j}}{h_{x}^{2}}; \quad C_{i} = A_{i} + B_{i} + m_{i,j} \frac{2}{\tau}; \quad F_{i} = m_{i,j} \frac{2}{\tau} H_{i,j}^{k-1}, \quad (F_{i,j}) = H_{i,j}^{k-\frac{2}{3}}, \quad (F_{i,j}) = H_{i,j}^{k+\frac{2}{3}}, \quad (F_$$

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Algorithm for computing one-dimensional problems with a conventional sweep [4]

$$\begin{aligned} \alpha_{0} &= \lambda_{1}; \quad \beta_{0} = (1 - \lambda_{1}), \\ i &= 0 \dots (N_{x} - 1), \quad i = 0 \dots (N_{y} - 1), \\ \alpha_{i+1} &= \frac{B_{i}}{C_{i} - \alpha_{i} \cdot A_{i}}, \quad \beta_{i+1} = \frac{A_{i} \cdot \beta_{i} + F_{i}}{C_{i} - \alpha_{i} \cdot A_{i}}, \\ i &= (N_{x} - 1) \dots 0, \quad i = (N_{y} - 1) \dots 0, \\ H_{N} &= \frac{(1 - \lambda_{2}) + \lambda_{2} \beta_{N}}{1 - \lambda_{2} \alpha_{N}}, \quad H_{i} = \alpha_{i+1} H_{i+1} + \beta_{i+1}. \end{aligned}$$

$$(10)$$

Now let us consider the algorithm for solving the problem by the stream sweep method in variants of schemes I-III.

To apply streaming run, we introduce the variable $w_x = K \frac{\partial H}{\partial x}$ $w_y = K \frac{\partial H}{\partial y}$.

Then (1) takes the following form:

$$\frac{\partial w_x}{\partial x} + \frac{\partial w_y}{\partial y} = m \frac{\partial H}{\partial t} + Q.$$
(11)

The finite-difference form of equation (11) when calculated using the longitudinal-transverse scheme is as follows:

$$\begin{pmatrix} w_{x_{i+\frac{1}{2},j}}^{k+\frac{1}{2}} - w_{x_{i+\frac{1}{2},j}}^{k+\frac{1}{2}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+\frac{1}{2}} + \frac{h}{\tau} F_{i}; \quad F_{i} = \tau \cdot \begin{pmatrix} w_{y_{j}}^{k} - w_{y_{j}}^{k} - w_{y_{j}}^{k} \\ Q_{i,j} - \frac{w_{y_{j}}^{k} - w_{y_{j}}^{k}}{h} \end{pmatrix} - m_{i,j} H_{i,j}^{k},$$

$$\begin{pmatrix} w_{y_{j}}^{k+1} - w_{y_{j}}^{k+1} \\ w_{y_{i,j+\frac{1}{2}}}^{k+1} - w_{y_{j+\frac{1}{2}}}^{k+1} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+1} + \frac{h}{\tau} F_{j}; \quad F_{j} = \tau \cdot \begin{pmatrix} Q_{i,j} - \frac{w_{x_{j}}^{k+1} - w_{y_{j}}^{k}}{h} \end{pmatrix} - m_{i,j} H_{i,j}^{k+\frac{1}{2}}.$$

$$(12)$$

The use of calculations of the locally one-dimensional scheme leads to the following form:

$$\begin{pmatrix} w_{x_{i+\frac{1}{2},j}}^{k+\frac{1}{2}} - w_{x_{i+\frac{1}{2},j}}^{k+\frac{1}{2}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+\frac{1}{2}} + \frac{h}{\tau} F_{i}; \quad F_{i} = \tau \cdot Q_{i,j} - m_{i,j} H_{i,j}^{k},$$

$$\begin{pmatrix} w_{y_{i,j+\frac{1}{2}}}^{k+1} - w_{y_{i,j-\frac{1}{2}}}^{k+1} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+1} + \frac{h}{\tau} F_{j}; \quad F_{j} = \tau \cdot Q_{i,j} - m_{i,j} H_{i,j}^{k+\frac{1}{2}}.$$

$$(13)$$

Now we give the sequences by the splitting method:

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$$\begin{pmatrix} w_{i+\frac{1}{2},j}^{k-\frac{2}{3}} - w_{i-\frac{1}{2},j}^{k-\frac{2}{3}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k-\frac{2}{3}} + \frac{h}{\tau} (F_i) \quad F_i = m_{i,j} H_{i,j}^{k-1}, \\ \begin{pmatrix} w_{i,j+\frac{1}{2}}^{k-\frac{1}{3}} - w_{i,j-\frac{1}{2}}^{k-\frac{1}{3}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k-\frac{1}{3}} + \frac{h}{\tau} (F_j) \quad F_j = m_{i,j} H_{i,j}^{k-\frac{2}{3}}, \\ H_{i,j}^{k+\frac{1}{3}} = H_{i,j}^{k-\frac{1}{3}} + 2 \cdot \tau \cdot Q_{i,j}, \\ \begin{pmatrix} w_{i,j+\frac{1}{2}}^{k+\frac{2}{3}} - w_{i,j-\frac{1}{2}}^{k+\frac{2}{3}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+\frac{2}{3}} + \frac{h}{\tau} (F_j) \quad F_j = m_{i,j} H_{i,j}^{k+\frac{1}{3}}, \\ \begin{pmatrix} w_{i,j+\frac{1}{2}}^{k+\frac{2}{3}} - w_{i,j-\frac{1}{2}}^{k+\frac{2}{3}} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+\frac{2}{3}} + \frac{h}{\tau} (F_j) \quad F_j = m_{i,j} H_{i,j}^{k+\frac{2}{3}}, \\ \begin{pmatrix} w_{i+\frac{1}{2},j}^{k+1} - w_{i,j-\frac{1}{2}}^{k+1} \end{pmatrix} = m_{i,j} \frac{h}{\tau} H_{i,j}^{k+1} + \frac{h}{\tau} (F_i) \quad F_i = m_{i,j} H_{i,j}^{k+\frac{2}{3}}. \end{cases}$$

To calculate (12) - (14) by the stream sweep method [4], we use an algorithm of the following form:

$$\begin{aligned} \alpha_{N} &= \frac{-\lambda_{2}}{0.5 \cdot \lambda_{2} + (1 - \lambda_{2})}, \qquad \beta_{N} = \frac{\lambda_{2} - 0.5 \cdot \lambda_{2} * F_{N}}{0.5 \cdot \lambda_{2} + (1 - \lambda_{2})}, \\ i &= (N_{x} - 1) \dots 0, \quad i = (N_{y} - 1) \dots 0, \\ \alpha_{i} &= \frac{\frac{h^{2}}{\tau} - \alpha_{i+1}}{1 + \frac{h^{2}}{\tau} - \alpha_{i+1}}, \qquad \beta_{i} = \frac{\beta_{i+1} - F_{i} \left(\frac{h^{2}}{\tau} - \alpha_{i+1}\right)}{1 + \frac{h^{2}}{\tau} - \alpha_{i+1}}, \\ H_{0} &= \frac{\frac{h}{\tau} \cdot \lambda_{1} \cdot \beta_{0} - \gamma_{1} \cdot \left(\alpha_{0} - \frac{h^{2}}{\tau}\right) - 0.5 \frac{h}{\tau} \lambda_{1} \cdot F_{0} \cdot \left(\alpha_{0} - \frac{h^{2}}{\tau}\right)}{\left((1 - \lambda_{1}) - 0.5 \cdot \frac{h}{\tau} \lambda_{1}\right) \cdot \left(\alpha_{0} - \frac{h^{2}}{\tau}\right) + \frac{h}{\tau} \lambda_{1}}, \\ i &= 0 \dots (N_{x} - 1), \quad i = 0 \dots (N_{y} - 1), \\ H_{i+1} &= \left(\frac{\alpha_{i+1}}{\frac{h^{2}}{\tau} - \alpha_{i+1}}\right) \cdot \left(\beta_{i+1} - H_{i}\right) + \beta_{i+1}. \end{aligned}$$
(15)

4. COMPUTATIONAL EXPERIMENT.

Let's check the accuracy of the algorithms created using the data given below. Let's create results for each method using programs using the Delphi programming language. An oil reservoir has a length and width $0 \le x, y \le 1000 \text{ M}$, constant thickness h = 50 M, viscosity $\mu = 2$ and initial reservoir pressure $P_0 = 25 \text{ Atm}$.

The reservoir is being developed by 5 wells. Table 1 shows the pressure field at t = 1800 days.

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ISSN: 2249-7137 Vol. 11, Issue 12, December 2021 SJIF 2021 = 7.492 A peer reviewed journal

TABLE 1							
25.00	25.00	24.99	24.96	24.97	25.00	25.00	25.00
25.00	24.98	24.83	24.81	24.83	25.00	25.00	25.00
24.99	24.84	23.77	24.49	23.77	24.83	24.97	25.00
24.99	24.82	24.49	22.96	24.49	24.82	24.96	25.00
25.00	24.84	23.77	24.49	23.78	24.86	24.99	25.00
25.00	24.95	24.82	24.81	24.84	25.00	25.00	25.00
25.00	25.00	24.97	24.96	24.97	25.00	25.00	25.00

Figure 1 shows the view of the considered region D, and Fig. 2 shows the isoline of the pressure field at t = 1800 days.





Figure 2. Isoline of the pressure field at t = 1800 days.

5. CONCLUSION

In conclusion, the most effective way to calculate the problem of two-dimensional liquid filtration is to apply the flow drive to the locally one-dimensional scheme. Because by applying this combination it is possible to reduce the calculation time by reducing the calculations and results close to other methods are achieved.

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